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ORGANOSOLS COMPRISING A CHROMOPHORE, METHODS AND USES

FIELD OF THE INVENTION

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The present invention relates to organosols comprising a chromophore. More specifically, the present invention relates to organosols having a chromophore covalently linked thereto by a urethane linkage.

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BACKGROUND

In electrophotographic and electrostatic printing processes (collectively electrographic processes), an electrostatic image is formed on the surface of a photoreceptive element or dielectric element, respectively. The photoreceptive element or dielectric element may be an intermediate transfer drum or belt or the substrate for the final toned image itself, as described by Schmidt, S. P. and Larson, J. R. in Handbook of Imaging Materials Diamond, A. S., Ed: Marcel Dekker: New York; Chapter 6, pp 227-252, and U.S. Pat. Nos. 4,728,983, 4,321,404, and 4,268,598.

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In electrostatic printing, a latent image is typically formed by (1) placing a charge image onto a dielectric element (typically the receiving substrate) in selected areas of the element with an electrostatic writing stylus or its equivalent to form a charge image, (2) applying toner to the charge image, and (3) fixing the toned image. An example of this type of process is described in U.S. Pat. No. 5,262,259.

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In electrophotographic printing, also referred to as xerography, electrophotographic technology is used to produce images on a final image receptor, such as paper, film, or the like. Electrophotographic technology is incorporated into a wide

range of equipment including photocopiers, laser printers, facsimile machines, and the like.

Electrophotography typically involves the use of a reusable, light sensitive, temporary image receptor, known as a photoreceptor, in the process of producing an electrophotographic image on a final, permanent image receptor. A representative electrophotographic process involves a series of steps to produce an image on a receptor, including charging, exposure, development, transfer, fusing, and cleaning, and erasure.

In the charging step, a photoreceptor is covered with charge of a desired polarity, either negative or positive, typically with a corona or charging roller. In the exposure step, an optical system, typically a laser scanner or diode array, forms a latent image by selectively discharging the charged surface of the photoreceptor in an imagewise manner corresponding to the desired image to be formed on the final image receptor. In the development step, toner particles of the appropriate polarity are generally brought into contact with the latent image on the photoreceptor, typically using a developer electrically-biased to a potential opposite in polarity to the toner polarity. The toner particles migrate to the photoreceptor and selectively adhere to the latent image via electrostatic forces, forming a toned image on the photoreceptor.

In the transfer step, the toned image is transferred from the photoreceptor to the desired final image receptor; an intermediate transfer element is sometimes used to effect transfer of the toned image from the photoreceptor with subsequent transfer of the toned image to a final image receptor. In the fusing step, the toned image on the final image receptor is heated to soften or melt the toner particles, thereby fusing the toned image to the final receptor. An alternative fusing method involves fixing the toner to the final receptor under high pressure with or without heat. In the cleaning step, residual toner remaining on the photoreceptor is removed.

Finally, in the erasing step, the photoreceptor charge is reduced to a substantially uniformly low value by exposure to light of a particular wavelength band, thereby removing remnants of the original latent image and preparing the photoreceptor for the next imaging cycle.

Two types of toner are in widespread, commercial use: liquid toner and dry toner. The term "dry" does not mean that the dry toner is totally free of any liquid constituents,

but connotes that the toner particles do not contain any significant amount of solvent, e.g., typically less than 10 weight percent solvent (generally, dry toner is as dry as is reasonably practical in terms of solvent content), and are capable of carrying a triboelectric charge. This distinguishes dry toner particles from liquid toner particles in 5 that liquid toner particles are solvatable to some degree, typically in more than 50 weight percent of a low polarity, low dielectric carrier solvent; and liquid toner particles are generally chemically charged using polar groups that dissociate in the carrier solvent, but do not carry a triboelectric charge while solvated and/or dispersed in the liquid carrier.

A typical dry toner particle generally comprises a polymeric binder and optionally 10 a visual enhancement additive, e.g., a colored pigment particle. The binder fulfills functions both during and after the electrophotographic process. With respect to processability, the character of the binder impacts the triboelectric charging and charge retention characteristics, flow, and fusing characteristics of the toner particles. These characteristics are important to achieve good performance during development, transfer, 15 and fusing. After an image is formed on the final receptor, the nature of the binder (e.g. glass transition temperature, melt viscosity, molecular weight) and the fusing conditions (e.g. temperature, pressure and fuser configuration) impact durability (e.g. blocking and erasure resistance), adhesion to the receptor, gloss, and the like.

For example, polymeric materials suitable for use in dry toner particles typically 20 have a high glass transition temperature (T_g) of at least about 50-65°C in order to obtain good blocking resistance after fusing, yet typically require high fusing temperatures of about 200-250°C in order to soften or melt the toner particles and thereby adequately fuse the toner to the final image receptor. High fusing temperatures are a disadvantage for dry toner because of the long warm-up time and higher energy consumption associated with 25 high temperature fusing and because of the risk of fire associated with fusing toner to paper at temperatures approaching the autoignition temperature of paper (233°C).

In addition, some dry toners using high T_g polymeric binders are known to exhibit undesirable partial transfer (offset) of the toned image from the final image receptor to the fuser surface at temperatures above or below the optimal fusing temperature, 30 requiring the use of low surface energy materials in the fuser surface or the application of fuser oils to prevent offset. Alternatively, various lubricants or waxes have been

physically blended into the dry toner particles during fabrication to act as release or slip agents; however, because these waxes are not chemically bonded to the polymeric binder, they may adversely affect triboelectric charging of the toner particle or may migrate from the toner particle and contaminate the photoreceptor, an intermediate transfer element, 5 the fuser element, or other surfaces critical to the electrophotographic process. In addition to the visual enhancement additive and the polymeric binder, dry toner particles may optionally include other additives.

Charge control additives (charge directors, charge control agents or CCA's) are often used in dry toner when the other ingredients, by themselves, do not provide the 10 desired triboelectric charging or charge retention properties. As noted above, release or slip agents may be used to help prevent the toner from sticking to fuser rolls when those are used, thereby preventing or reducing offset. Other additives include antioxidants, ultraviolet stabilizers, fungicides, bactericides, flow control agents, and the like.

Dry toner particles have been manufactured using a wide range of fabrication 15 techniques. One widespread fabrication technique involves melt mixing the ingredients, comminuting the solid blend that results to form particles, and then classifying the resultant particles to remove fines and larger material of unwanted particle size. External additives may then be blended with the resultant particles. This approach has drawbacks. First, the approach necessitates the use of polymeric binder materials that are friable or 20 fracturable to some degree so that comminution can be carried out. This limits the kinds of polymeric materials that can be used, including materials that are fracture resistant and highly durable. This also limits the kinds of colorants to be used, in that some materials such as metal flakes, or the like, may tend to be damaged to too large a degree by the energy encountered during comminution.

25 The amount of energy required by comminution itself is a drawback in terms of equipment demands and associated manufacturing expenses. Also, material usage is inefficient in that fines and larger particles are unwanted and must be screened out from the desired product. In short, significant material is wasted. Recycling of unused material is not always practical to reduce such waste inasmuch as the composition of 30 recycled material may tend to shift from what is desired.

Relatively recently, chemically grown dry toner materials have been made using a variety of methods. In such methods, the polymeric binder is typically manufactured as a dispersion in aqueous media by solution, suspension, or emulsion polymerization techniques under conditions that form monodisperse, polymeric particles that are fairly uniform in size and shape. After the polymeric binder is formed, it is filtered and washed to remove unreacted monomer, surfactants and other extraneous material, then dried and combined with other desired ingredients to form a dry toner powder. Because the high boiling point and large latent heat of vaporization of water makes it impractical and expensive to evaporate all of the aqueous media to obtain a dry polymeric binder, drying of the binder is often effected by filtration to remove a substantial amount of the water, followed by evaporative drying to remove substantially all of the remaining aqueous media.

A typical liquid toner composition generally includes toner particles suspended or dispersed in a liquid carrier. The liquid carrier is typically nonconductive dispersant, to avoid discharging the latent electrostatic image.

Liquid toner particles are generally solvated to some degree in the liquid carrier (or carrier liquid), typically in more than 50 weight percent of a low polarity, low dielectric constant, substantially nonaqueous carrier solvent. Liquid toner particles are generally chemically charged using polar groups that dissociate in the carrier solvent, but do not carry a triboelectric charge while solvated and/or dispersed in the liquid carrier. Liquid toner particles are also typically smaller than dry toner particles. Because of their small particle size, ranging from about 5 microns to sub-micron, liquid toners are capable of producing very high-resolution toned images.

A typical toner particle for a liquid toner composition generally comprises a visual enhancement additive (for example, a colored pigment particle) and a polymeric binder. The polymeric binder fulfills functions both during and after the electrophotographic process. With respect to processability, the character of the binder impacts charging and charge stability, flow, and fusing characteristics of the toner particles. These characteristics are important to achieve good performance during development, transfer, and fusing. After an image is formed on the final receptor, the nature of the binder (e.g. glass transition temperature, melt viscosity, molecular weight)

and the fusing conditions (e.g. temperature, pressure and fuser configuration) impact durability (e.g. blocking and erasure resistance), adhesion to the receptor, gloss, and the like.

Polymeric binder materials suitable for use in liquid toner particles typically 5 exhibit glass transition temperatures of about -24°C to 55°C, which is lower than the range of glass transition temperatures (50-100°C) typical for polymeric binders used in dry toner particles. In particular, some liquid toners are known to incorporate polymeric binders exhibiting glass transition temperatures (T_g) below room temperature (25°C) in order to rapidly self fix, e.g., by film formation, in the liquid electrophotographic imaging 10 process; see e.g. U.S. 6,255,363. However, such liquid toners are also known to exhibit inferior image durability resulting from the low T_g (e.g. poor blocking and erasure resistance) after fusing the toned image to a final image receptor.

In other printing processes using liquid toners, self-fixing is not required. In such a system, the image developed on the photoconductive surface is transferred to an 15 intermediate transfer belt ("ITB") or intermediate transfer member ("ITM") or directly to a print medium without film formation at this stage. See, for example, U.S. Patent Nos. 5,410,392 to Landa, issued on April 25, 1995; and 5,115,277 to Camis, issued on May 19, 1992. In such a system, this transfer of discrete toner particles in image form is carried out using a combination of mechanical forces, electrostatic forces, and thermal 20 energy. In the system particularly described in the '277 patent, DC bias voltage is connected to an inner sleeve member to develop electrostatic forces at the surface of the print medium for assisting in the efficient transfer of color images.

The toner particles used in such a system have been previously prepared using conventional polymeric binder materials, and not polymers made using an organosol 25 process. Thus, for example the '392 patent states that the liquid developer to be used in the disclosed system is described in U. S. Patent No. 4,794,651 to Landa, issued on December 27, 1988. This patent discloses liquid toners made by heating a preformed high T_g polymer resin in a carrier liquid to an elevated temperature sufficiently high for the carrier liquid to soften or plasticize the resin, adding a pigment, and exposing the 30 resulting high temperature dispersion to a high energy mixing or milling process.

Although such non self-fixing liquid toners using higher T_g (T_g generally greater than or equal to about 60°C) polymeric binders should have good image durability, such toners are known to exhibit other problems related to the choice of polymeric binder, including image defects due to the inability of the liquid toner to rapidly self fix in the imaging process, poor charging and charge stability, poor stability with respect to agglomeration or aggregation in storage, poor sedimentation stability in storage, and the requirement that high fusing temperatures of about 200-250°C be used in order to soften or melt the toner particles and thereby adequately fuse the toner to the final image receptor.

To overcome the durability deficiencies, polymeric materials selected for use in both nonfilm-forming liquid toners and dry toners more typically exhibit a range of T_g of at least about 55-65°C in order to obtain good blocking resistance after fusing, yet typically require high fusing temperatures of about 200-250°C in order to soften or melt the toner particles and thereby adequately fuse the toner to the final image receptor.

Solvent-based polymer dispersions in a nonaqueous liquid (organosols) have been prepared using dispersion polymerization in low polarity, low dielectric constant carrier solvents for use in making relatively low glass transition temperature ($T_g \leq 30^\circ\text{C}$) film-forming liquid electrophotographic toners. See, e.g., U.S. Pat. No. 5,886,067 and 6,103,781. Organosols have also been prepared for use in making intermediate glass transition temperature (T_g 30-55°C) liquid electrostatic toners for use in electrostatic stylus printers. See e.g. U.S. Pat. No. 6,255,363 B1.

Some solvent-based polymer dispersions have also been developed for producing dry toners. See, e.g., U.S. Pat. Nos. 6,136,490 and 5,384,226 and Japanese Published Patent Document No. 05-119529. Unfortunately, the use of organosols or solvent-based polymer dispersion to make dry toner particles has proved to be substantially more challenging than the use of organosols to make liquid toner compositions. When a solvent-based dispersion is dried to remove the nonaqueous liquid carrier as is necessary to make dry toner particles, the binder particles tend to agglomerate and/or aggregate into one or more large masses. Such masses must be pulverized or otherwise comminuted in order to obtain dry toner particles of an appropriate size. The need for such comminution defeats a major advantage of using organosols in the first instance, which is the formation

of substantially monodisperse, polymeric particles of uniform size and shape. In addition, it has been reported to be more difficult to incorporate slip agents (e.g. waxes) or triboelectric charge control additives (CCA's) into nonaqueous dispersions due to solubility constraints and other considerations. Consequently, the full spectrum of 5 benefits that result from using organosols has not been realized for widespread, commercial, dry toner applications.

Particle size and charge characteristics are especially important to form high quality images with good resolution using toners. Toner particles must be as uniform in size, charge rate, and charge holding characteristics as is practically possible in order to 10 maximize image forming performance. Accordingly, there is always a demand in this industry for techniques that yield toner particles with more uniform particle size, charging rate, and/or charge holding characteristics. There is also a demand for new polymeric binders for toners that exhibit controllable particle size, shape and charge polarity; improved charging characteristics and charge stability; improved low 15 temperature fusing performance; and lower manufacturing cost arising from improved yields, reduced processing steps, or more efficient processing methods.

U.S. Patent No. 5,663,024 to Smith describes liquid toners for electrophotography comprising polymeric dyes. In these toners, the polymeric dye contains macromeric moieties that render the polymeric dye dispersible in hydrocarbon solvents and 20 additionally contains segments that impart color. The polymeric dye may contain either a charge-directing chelating moiety or a surface-release promoting moiety, or both of these moieties. Polymeric dyes as described therein are classified in two classes: (1) backbone polymeric dyes and (2) pendent polymeric dyes. Smith further states that there are two general methods for preparing pendent polymeric dyes: (1) the polymerization of a 25 monomer containing a pendent chromophore, and (2) the reaction of a pre-formed polymer with a reactive dye or reactive dye developer. The dyes produced by method (1) are stated to be typically made by copolymerization of a free radically polymerizable monomer having a chromophore and a colorless free radically polymerizable monomer. Suitable free radically polymerizable monomers containing a chromophore are stated to 30 be known in the art, citing U.S. Pat. No. 4,614,521 section [D] as disclosing "sublimable

dyes having an acryloyl or a methacryloyl group." Another list of dyes containing acryloyl or methacryloyl groups are stated to be found in U.S. Pat. No. 4,795,794.

Reactive colorants for use in polyurethane resins are described in US Patent No. 4,775,748 to Kluger, assigned to Milliken Research Corporation. These colorants are disclosed to be incorporated into resin during the formation of polyurethanes. The products of the invention as disclosed are stated to be particularly useful for production of colored polyurethane foams. Additionally, Reactint® Colorants are sold by Milliken Chemical and are described on their website at http://www.millikenchemical.com/html/reac_f.html as polyols to which color molecules are attached, based on a technology proprietary to Milliken Chemical. These materials are stated to be the most widely used products for coloring polyurethane in the world.

SUMMARY OF THE INVENTION

The present invention relates to amphipathic copolymers comprising one or more S portions and one or more D portions. The copolymers have a chromophore covalently bonded thereto via a urethane, urea or amide linkage. These copolymers provide exceptionally useful components in toner compositions, because they provide easily prepared color-imparting particles that provide excellent color rendition. More specifically, it has been found that chromophores may be easily covalently bonded to amphipathic copolymers through chemical linkages that are resilient. Thus, colored particles of the present invention exhibit good performance properties even when exposed to shear conditions, such as may be required under handling or milling operations, for example to reduce agglomerations or particle size. Advantageously, it has been found that there is a wide availability of reactive dyes suitable for incorporation into the amphipathic copolymers of the present invention. Further many dyes either contain the desired reactive functionalities or may be readily modified to incorporate the desired reactive functionality, with the final particle exhibiting little or no color shift from the starting dye material. Thus, toner compositions may be readily prepared in accordance with the present invention using off-the-shelf, or near off-the-shelf dye materials.

Additionally, because many suitable dye starting materials are available, it is possible to readily select non-toxic and non hazardous starting materials for preparation of the toners of the present invention.

As a particular advantage, the amphipathic copolymer comprising covalently bonded chromophores of the present invention do not require the use of pigment in the ultimate toner composition. Conventionally, pigments are used in toner compositions to provide the desired color rendition of the toner, and to produce the desired image. Pigments previously have been physically associated with the amphipathic copolymer by subjecting the copolymer to one or more high energy mixing processes. The dispersed copolymer or fragments derived from the copolymer then associate with the pigment particle, for example, by adsorbing to or adhering to the surface of the pigment. By use of the present invention, this high energy mixing process may be reduced or eliminated. Further, because the chromophore is covalently bonded to the amphipathic copolymer, the toner composition may be more stable, because no pigment will be dissociated from the amphipathic copolymer. Toners of the present invention that do not contain pigments therefore do not experience pigment separation from the binder. This is particularly beneficial in liquid toner embodiments, where sedimentation of pigment out of the toner composition may be a problem, particularly over long term storage of the toner product. Optionally, additional visual enhancement additives may be provided in the toner compositions of the present invention if desired. Incorporation of such additives, particularly pigments, may be desirable in certain embodiments where enhanced hiding power of the toner is required.

In a preferred embodiment of the present invention, amphipathic copolymers are prepared wherein a single color of chromophore is covalently bonded to the copolymer to provide a predetermined color. In another preferred embodiment of the present invention, amphipathic copolymers are prepared wherein a plurality of chromophores having different colors are covalently bonded to the copolymer to provide a predetermined blended color. Toner compositions thus can be prepared to provide excellent color renditions by providing a composition having only one type of chromophore present in the toner composition. Alternatively, the toner composition may comprise a plurality chromophores blended in a predetermined ratio to provide a toner

composition having a predetermined blended color. These chromophores in one embodiment may be provided as a prereacted blend on each amphipathic copolymer (i.e. that each copolymer exhibits substantially the same color blend). Alternatively, chromophores of different colors may be reacted with separate amphipathic copolymers, 5 with subsequent blending of the copolymers in predetermined ratios to exhibit the desired predetermined toner composition color.

As used herein, the term "amphipathic" is well known and refers to a copolymer having a combination of portions having distinct solubility and dispersibility characteristics, respectively, in a desired liquid carrier that is used to make the copolymer 10 and/or used in the course of incorporating the copolymer into the dry toner particles. Preferably, the liquid carrier is selected such that at least one portion (also referred to herein as S material or portion(s)) of the copolymer is more solvated by the carrier while at least one other portion (also referred to herein as D material or portion(s)) of the copolymer constitutes more of a dispersed phase in the carrier.

15 In preferred embodiments, the copolymer is polymerized *in situ* in the desired substantially nonaqueous liquid carrier as this yields monodisperse copolymeric particles suitable for use in toner with little, if any, need for subsequent comminuting or classifying. The resulting organosol may optionally be mixed with visual enhancement additives and/or one or more other desired ingredients. During such combination, 20 ingredients comprising the visual enhancement particles and the amphipathic copolymer will tend to self-assemble into composite toner particles. Specifically, it is believed that the D portion of the copolymer will tend to physically and/or chemically interact with the surface of the visual enhancement additive, while the S portion helps promote dispersion in the carrier without use of a separate surfactant or dispersant. In the case of dry toner 25 embodiments of the present invention, the dispersion is then dried to the desired degree to provide composite dry toner particles, preferably using the fluidized drying techniques described herein.

DETAILED DESCRIPTION OF PRESENTLY PREFERRED EMBODIMENTS

5 The embodiments of the present invention described below are not intended to be exhaustive or to limit the invention to the precise forms disclosed in the following detailed description. Rather the embodiments are chosen and described so that others skilled in the art may appreciate and understand the principles and practices of the present
10 invention.

Preferably, the nonaqueous liquid carrier of the organosol is selected such that at least one portion (also referred to herein as the S material or portion) of the amphipathic copolymer is more solvated by the carrier while at least one other portion (also referred to herein as the D material or portion) of the copolymer constitutes more of a dispersed phase in the carrier. Preferred copolymers of the present invention comprise S and D material having respective solubilities in the desired liquid carrier that are sufficiently different from each other such that the S blocks tend to be more solvated by the carrier while the D blocks tend to be more dispersed in the carrier. More preferably, the S blocks are soluble in the liquid carrier while the D blocks are insoluble. In particularly preferred embodiments, the D material phase separates from the liquid carrier, forming dispersed particles.
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From one perspective, the polymer particles when dispersed in the liquid carrier may be viewed as having a core/shell structure in which the D material tends to be in the core, while the S material tends to be in the shell. The S material thus functions as a dispersing aid, steric stabilizer or graft copolymer stabilizer, to help stabilize dispersions of the copolymer particles in the liquid carrier. Consequently, the S material may also be referred to herein as a "graft stabilizer." The core/shell structure of the binder particles tends to be retained when the particles are dried and when incorporated into dry toner particles.
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30 The solubility of a material, or a portion of a material such as a copolymeric portion, may be qualitatively and quantitatively characterized in terms of its Hildebrand

solubility parameter. The Hildebrand solubility parameter refers to a solubility parameter represented by the square root of the cohesive energy density of a material, having units of $(\text{pressure})^{1/2}$, and being equal to $(\Delta H/RT)^{1/2} / V^{1/2}$, where ΔH is the molar vaporization enthalpy of the material, R is the universal gas constant, T is the absolute temperature, and V is the molar volume of the solvent. Hildebrand solubility parameters are tabulated for solvents in Barton, A. F. M., Handbook of Solubility and Other Cohesion Parameters, 2d Ed. CRC Press, Boca Raton, Fla., (1991), for monomers and representative polymers in Polymer Handbook, 3rd Ed., J. Brandrup & E. H. Immergut, Eds. John Wiley, N.Y., pp 519-557 (1989), and for many commercially available polymers in Barton, A. F. M., Handbook of Polymer-Liquid Interaction Parameters and Solubility Parameters, CRC Press, Boca Raton, Fla., (1990).

The degree of solubility of a material, or portion thereof, in a liquid carrier may be predicted from the absolute difference in Hildebrand solubility parameters between the material, or portion thereof, and the liquid carrier. A material, or portion thereof, will be fully soluble or at least in a highly solvated state when the absolute difference in Hildebrand solubility parameter between the material, or portion thereof, and the liquid carrier is less than approximately $1.5 \text{ MPa}^{1/2}$. On the other hand, when the absolute difference between the Hildebrand solubility parameters exceeds approximately $3.0 \text{ MPa}^{1/2}$, the material, or portion thereof, will tend to phase separate from the liquid carrier, forming a dispersion. When the absolute difference in Hildebrand solubility parameters is between $1.5 \text{ MPa}^{1/2}$ and $3.0 \text{ MPa}^{1/2}$, the material, or portion thereof, is considered to be weakly solvatable or marginally insoluble in the liquid carrier.

Consequently, in preferred embodiments, the absolute difference between the respective Hildebrand solubility parameters of the S portion(s) of the copolymer and the liquid carrier is less than $3.0 \text{ MPa}^{1/2}$, preferably less than about $2.0 \text{ MPa}^{1/2}$, more preferably less than about $1.5 \text{ MPa}^{1/2}$. In a particularly preferred embodiment of the present invention, the absolute difference between the respective Hildebrand solubility parameters of the S portion(s) of the copolymer and the liquid carrier is from about 2 to about $3.0 \text{ MPa}^{1/2}$. Additionally, it is also preferred that the absolute difference between the respective Hildebrand solubility parameters of the D portion(s) of the copolymer and the liquid carrier is greater than $2.3 \text{ MPa}^{1/2}$, preferably greater than about $2.5 \text{ MPa}^{1/2}$,

more preferably greater than about 3.0 MPa^{1/2}, with the proviso that the difference between the respective Hildebrand solubility parameters of the S and D portion(s) is at least about 0.4 MPa^{1/2}, more preferably at least about 1.0 MPa^{1/2}. Because the Hildebrand solubility of a material may vary with changes in temperature, such solubility 5 parameters are preferably determined at a desired reference temperature such as at 25°C.

Those skilled in the art understand that the Hildebrand solubility parameter for a copolymer, or portion thereof, may be calculated using a volume fraction weighting of the individual Hildebrand solubility parameters for each monomer comprising the copolymer, or portion thereof, as described for binary copolymers in Barton A. F. M., 10 Handbook of Solubility Parameters and Other Cohesion Parameters, CRC Press, Boca Raton, p 12 (1990). The magnitude of the Hildebrand solubility parameter for polymeric materials is also known to be weakly dependent upon the weight average molecular weight of the polymer, as noted in Barton, pp 446-448. Thus, there will be a preferred molecular weight range for a given polymer or portion thereof in order to achieve desired 15 solvating or dispersing characteristics. Similarly, the Hildebrand solubility parameter for a mixture may be calculated using a volume fraction weighting of the individual Hildebrand solubility parameters for each component of the mixture.

In addition, we have defined our invention in terms of the calculated solubility parameters of the monomers and solvents obtained using the group contribution method 20 developed by Small, P. A., J. Appl. Chem., 3, 71 (1953) using Small's group contribution values listed in Table 2.2 on page VII/525 in the Polymer Handbook, 3rd Ed., J. Brandrup & E. H. Immergut, Eds. John Wiley, New York, (1989). We have chosen this method for defining our invention to avoid ambiguities which could result from using solubility parameter values obtained with different experimental methods. In addition, Small's 25 group contribution values will generate solubility parameters that are consistent with data derived from measurements of the enthalpy of vaporization, and therefore are completely consistent with the defining expression for the Hildebrand solubility parameter. Since it is not practical to measure the heat of vaporization for polymers, monomers are a reasonable substitution.

30 For purposes of illustration, Table I lists Hildebrand solubility parameters for some common solvents used in an electrophotographic toner and the Hildebrand

solubility parameters and glass transition temperatures (based on their high molecular weight homopolymers) for some common monomers used in synthesizing organosols.

TABLE I

Hildebrand Solubility Parameters Solvent Values at 25°C		
Solvent Name	Kauri-Butanol Number by ASTM Method D1133- 54T (ml)	Hildebrand Solubility Parameter (MPa ^{1/2})
Norpar™ 15	18	13.99
Norpar™ 13	22	14.24
Norpar™ 12	23	14.30
Isopar™ V	25	14.42
Isopar™ G	28	14.60
Exxsol™ D80	28	14.60

Source: Calculated from equation #31 of Polymer Handbook, 3rd Ed., J. Brandrup E. H. Immergut, Eds. John Wiley, NY, p. VII/522 (1989).

Monomer Values at 25°C		
Monomer Name	Hildebrand Solubility Parameter (MPa ^{1/2})	Glass Transition Temperature (°C)*
3,3,5-Trimethyl Cyclohexyl Methacrylate	16.73	125
Isobornyl Methacrylate	16.90	110
Isobornyl Acrylate	16.01	94
n-Behenyl acrylate	16.74	< -55 (58 m.p.)**
n-Octadecyl Methacrylate	16.77	-100 (45 m.p.) **
n-Octadecyl Acrylate	16.82	-55
Lauryl Methacrylate	16.84	-65
Lauryl Acrylate	16.95	-30
2-Ethylhexyl Methacrylate	16.97	-10
2-Ethylhexyl Acrylate	17.03	-55
n-Hexyl Methacrylate	17.13	-5
t-Butyl Methacrylate	17.16	107
n-Butyl Methacrylate	17.22	20
n-Hexyl Acrylate	17.30	-60
n-Butyl Acrylate	17.45	-55
Ethyl Methacrylate	17.62	65
Ethyl Acrylate	18.04	-24
Methyl Methacrylate	18.17	105
Styrene	18.05	100

Calculated using Small's Group Contribution Method, Small, P.A. Journal of Applied Chemistry 3 p. 71 (1953). Using Group Contributions from Polymer Handbook, 3rd Ed., J. Brandrup E. H. Immergut, Eds., John Wiley, NY, p. VII/525 (1989).

*Polymer Handbook, 3rd Ed., J. Brandrup E. H. Immergut, Eds., John Wiley, NY, pp. VII/209-277 (1989). The T_g listed is for the homopolymer of the respective monomer.

** m.p. refers to melting point for selected Polymerizable Crystallizable Compounds.

The liquid carrier is a substantially nonaqueous solvent or solvent blend. In other words, only a minor component (generally less than 25 weight percent) of the liquid carrier comprises water. Preferably, the substantially nonaqueous liquid carrier

5 comprises less than 20 weight percent water, more preferably less than 10 weight percent water, even more preferably less than 3 weight percent water, most preferably less than one weight percent water.

The substantially nonaqueous carrier liquid may be selected from a wide variety of materials, or combination of materials, which are known in the art, but preferably has a

10 Kauri-butanol number less than 30 ml. The liquid is preferably oleophilic, chemically stable under a variety of conditions, and electrically insulating. Electrically insulating refers to a dispersant liquid having a low dielectric constant and a high electrical resistivity. Preferably, the liquid dispersant has a dielectric constant of less than 5; more preferably less than 3. Electrical resistivities of carrier liquids are typically greater than

15 10^9 Ohm-cm; more preferably greater than 10^{10} Ohm-cm. In addition, the liquid carrier desirably is chemically inert in most embodiments with respect to the ingredients used to formulate the toner particles.

Examples of suitable liquid carriers include aliphatic hydrocarbons (n-pentane, hexane, heptane and the like), cycloaliphatic hydrocarbons (cyclopentane, cyclohexane and the like), aromatic hydrocarbons (benzene, toluene, xylene and the like), halogenated hydrocarbon solvents (chlorinated alkanes, fluorinated alkanes, chlorofluorocarbons and the like) silicone oils and blends of these solvents. Preferred carrier liquids include branched paraffinic solvent blends such as IsoparTM G, IsoparTM H, IsoparTM K, IsoparTM L, IsoparTM M and IsoparTM V (available from Exxon Corporation, NJ), and most preferred carriers are the aliphatic hydrocarbon solvent blends such as NorparTM 12, NorparTM 13 and NorparTM 15 (available from Exxon Corporation, NJ). Particularly preferred carrier liquids have a Hildebrand solubility parameter of from about 13 to about 15 MPa^{1/2}.

As used herein, the term "copolymer" encompasses both oligomeric and

30 polymeric materials, and encompasses polymers incorporating two or more monomers. As used herein, the term "monomer" means a relatively low molecular weight material

(i.e., generally having a molecular weight less than about 500 Daltons) having one or more polymerizable groups. "Oligomer" means a relatively intermediate sized molecule incorporating two or more monomers and generally having a molecular weight of from about 500 up to about 10,000 Daltons. "Polymer" means a relatively large material

5 comprising a substructure formed two or more monomeric, oligomeric, and/or polymeric constituents and generally having a molecular weight greater than about 10,000 Daltons.

The term "macromer" or "macromonomer" refers to an oligomer or polymer having a terminal polymerizable moiety. "Polymerizable crystallizable compound" or "PCC" refers to compounds capable of undergoing polymerization to produce a polymer

10 portion capable of undergoing reversible crystallization over a reproducible and well-defined temperature range (e.g. the copolymer exhibits a melting and freezing point as determined, for example, by differential scanning calorimetry). PCC's may include monomers, functional oligomers, functional pre-polymers, macromers or other compounds able to undergo polymerization to form a polymer portion copolymer. The

15 term "molecular weight" as used throughout this specification means weight average molecular weight unless expressly noted otherwise.

The weight average molecular weight of the amphipathic copolymer of the present invention may vary over a wide range, and may impact imaging performance. The polydispersity of the copolymer also may impact imaging and transfer performance

20 of the resultant dry toner material. Because of the difficulty of measuring molecular weight for an amphipathic copolymer, the particle size of the dispersed copolymer (organosol) may instead be correlated to imaging and transfer performance of the resultant dry toner material. Generally, the volume mean particle diameter (D_v) of the dispersed graft copolymer particles, determined by laser diffraction particle size

25 measurement, should be in the range 0.1-100 microns, more preferably 0.5-50 microns, even more preferably 1.0-20 microns, and most preferably 3-10 microns.

In addition, a correlation exists between the molecular weight of the solvatable or soluble S portion of the graft copolymer, and the imaging and transfer performance of the resultant toner. Generally, the S portion of the copolymer has a weight average

30 molecular weight in the range of 1000 to about 1,000,000 Daltons, preferably 5000 to 400,000 Daltons, more preferably 50,000 to 300,000 Daltons. It is also generally

desirable to maintain the polydispersity (the ratio of the weight-average molecular weight to the number average molecular weight) of the S portion of the copolymer below 15, more preferably below 5, most preferably below 2.5. It is a distinct advantage of the present invention that copolymer particles with such lower polydispersity characteristics 5 for the S portion are easily made in accordance with the practices described herein, particularly those embodiments in which the copolymer is formed in the liquid carrier *in situ*.

The relative amounts of S and D portions in a copolymer can impact the solvating and dispersability characteristics of these portions. For instance, if too little of the S 10 portion(s) are present, the copolymer may have too little stabilizing effect to sterically-stabilize the organosol with respect to aggregation as might be desired. If too little of the D portion(s) are present, the small amount of D material may be too soluble in the liquid carrier such that there may be insufficient driving force to form a distinct, dispersed phase in the liquid carrier. The presence of both a solvated and dispersed phase helps the 15 ingredients of particles self assemble *in situ* with exceptional uniformity among separate particles. Balancing these concerns, the preferred weight ratio of D material to S material is in the range of 1:20 to 20:1, preferably 1:1 to 15:1, more preferably 2:1 to 10:1, and most preferably 4:1 to 8:1.

Glass transition temperature, T_g , refers to the temperature at which a (co)polymer, 20 or portion thereof, changes from a hard, glassy material to a rubbery, or viscous, material, corresponding to a dramatic increase in free volume as the (co)polymer is heated. The T_g can be calculated for a (co)polymer, or portion thereof, using known T_g values for the high molecular weight homopolymers (see, e.g., Table I herein) and the Fox equation expressed below:

25

$$1/T_g = w_1/T_{g1} + w_2/T_{g2} + \dots w_i/T_{gi}$$

wherein each w_n is the weight fraction of monomer "n" and each T_{gn} is the absolute glass 30 transition temperature (in degrees Kelvin) of the high molecular weight homopolymer of monomer "n" as described in Wicks, A. W., F. N. Jones & S. P. Pappas, *Organic Coatings 1*, John Wiley, NY, pp 54-55 (1992).

In the practice of the present invention, values of T_g for the D or S portion of the copolymer were determined using the Fox equation above, although the T_g of the copolymer as a whole may be determined experimentally using e.g. differential scanning calorimetry. The glass transition temperatures (T_g 's) of the S and D portions may vary
5 over a wide range and may be independently selected to enhance manufacturability and/or performance of the resulting dry toner particles. The T_g 's of the S and D portions will depend to a large degree upon the type of monomers constituting such portions. Consequently, to provide a copolymer material with higher T_g , one can select one or more higher T_g monomers with the appropriate solubility characteristics for the type of
10 copolymer portion (D or S) in which the monomer(s) will be used. Conversely, to provide a copolymer material with lower T_g , one can select one or more lower T_g monomers with the appropriate solubility characteristics for the type of portion in which the monomer(s) will be used.

For copolymers useful in dry toner applications, the copolymer T_g preferably
15 should not be too low or else receptors printed with the toner may experience undue blocking. Conversely, the minimum fusing temperature required to soften or melt the toner particles sufficient for them to adhere to the final image receptor will increase as the copolymer T_g increases. Consequently, it is preferred that the T_g of the copolymer be far enough above the expected maximum storage temperature of a printed receptor so as
20 to avoid blocking issues, yet not so high as to require fusing temperatures approaching the temperatures at which the final image receptor may be damaged, e.g. approaching the autoignition temperature of paper used as the final image receptor. In this regard, incorporation of a polymerizable crystallizable compound (PCC) in the copolymer will generally permit use of a lower copolymer T_g and therefore lower fusing temperatures
25 without the risk of the image blocking at storage temperatures below the melting temperature of the PCC. Desirably, therefore, the copolymer has a T_g of 0°-100°C, more preferably 20°-80°C, most preferably 40°-70°C.

The advantages of incorporating PCC's into the copolymer are further described in assignee's co-pending U.S. Patent Application titled **ORGANOSOL INCLUDING
30 AMPHIPATHIC COPOLYMERIC BINDER HAVING CRYSTALLINE MATERIAL, AND USE OF THE ORGANOSOL TO MAKE DRY TONER FOR**

ELECTROGRAPHIC APPLICATIONS, bearing Attorney Docket No. SAM0003/US, and filed on the same day as the present application in the names of **Julie Y. Qian et al.**, the co-pending patent application being incorporated herein by reference in its entirety.

For copolymers in which the D portion comprises a major portion of the 5 copolymer, the T_g of the D portion will dominate the T_g of the copolymer as a whole. For such copolymers useful in dry toner applications, it is preferred that the T_g of the D portion fall in the range of 20°-105°C, more preferably 30°-85°C, most preferably 60°-75°C, since the S portion will generally exhibit a lower T_g than the D portion, and a higher T_g D portion is therefore desirable to offset the T_g lowering effect of the S portion, 10 which may be solvatable. In this regard, incorporation of a polymerizable crystallizable compound (PCC) in the D portion of the copolymer will generally permit use of a lower D portion T_g and therefore lower fusing temperatures with reduced risk of image blocking at storage temperatures below the melting temperature of the PCC.

Blocking with respect to the S portion material is not as significant an issue 15 inasmuch as preferred copolymers comprise a majority of the D portion material. Consequently, the T_g of the D portion material will dominate the effective T_g of the copolymer as a whole. However, if the T_g of the S portion is too low, then the particles might tend to aggregate and/or aggregate during drying. On the other hand, if the T_g is 20 too high, then the requisite fusing temperature may be too high. Balancing these concerns, the S portion material is preferably formulated to have a T_g of at least 0°C, preferably at least 20°C, more preferably at least 40°C. In this regard, incorporation of a polymerizable crystallizable compound (PCC) in the S portion of the copolymer will generally permit use of a lower S portion T_g provided that the drying temperature used in forming the dry toner particles is maintained below the melting temperature of the PCC, 25 e.g. by using vacuum assisted drying, freeze drying, low temperature fluidized bed drying, and the like.

It is understood that the requirements imposed on the self-fixing characteristics of 30 a liquid toner will depend to a great extent upon the nature of the imaging process. For example, rapid self-fixing of the toner to form a cohesive film may not be required or even desired in an electrographic imaging process if the image is not subsequently transferred to a final receptor, or if the transfer is effected by means (e.g. electrostatic

transfer) not requiring a film formed toner on a temporary image receptor (e.g. a photoreceptor). Similarly, in multi-color (or multi-pass) electrostatic printing wherein a stylus is used to generate a latent electrostatic image directly upon a dielectric receptor that serves as the final toner receptor material, a rapidly self-fixing toner film may be
5 undesirably removed in passing under the stylus. This head scraping can be reduced or eliminated by manipulating the effective glass transition temperature of the organosol. For liquid electrographic (electrostatic) toners, particularly liquid toners developed for use in direct electrostatic printing processes, the D portion of the organosol is preferably provided with a sufficiently high T_g such that the organosol exhibits an effective glass
10 transition temperature of from about 15°C to about 55°C, and the D portion exhibits a T_g calculated using the Fox equation, of about 30-55°C. Liquid toners having both a polymerizable crystalline compound in the organosol and having an effective glass transition temperature of about 15-55 ° C provide particular benefit in the multipass electrostatic printing process as described above, because the toner exhibits both
15 excellent fusing temperature and superior resistance to marring or scraping either during or after the image is printed.

A wide variety of one or more different monomeric, oligomeric and/or polymeric materials may be independently incorporated into the S and D portions, as desired. Representative examples of suitable materials include free radically polymerized material
20 (also referred to as vinyl copolymers or (meth) acrylic copolymers in some embodiments), polyurethanes, polyester, epoxy, polyamide, polyimide, polysiloxane, fluoropolymer, polysulfone, combinations of these, and the like. Preferred S and D portions are derived from free radically polymerizable material. In the practice of the present invention, "free radically polymerizable " refers to monomers, oligomers, and/or
25 polymers having functionality directly or indirectly pendant from a monomer, oligomer, or polymer backbone (as the case may be) that participate in polymerization reactions via a free radical mechanism. Representative examples of such functionality includes (meth)acrylate groups, olefinic carbon-carbon double bonds, allyloxy groups, alpha-methyl styrene groups, (meth)acrylamide groups, cyanate ester groups, vinyl ether groups, combinations of these, and the like. The term "(meth)acryl", as used herein,
30 encompasses acryl and/or methacryl.

Free radically polymerizable monomers, oligomers, and/or polymers are advantageously used to form the copolymer in that so many different types are commercially available and may be selected with a wide variety of desired characteristics that help provide one or more desired performance characteristics. Free radically 5 polymerizable monomers, oligomers, and/or monomers suitable in the practice of the present invention may include one or more free radically polymerizable moieties.

Representative examples of monofunctional, free radically polymerizable monomers include styrene, alpha-methylstyrene, substituted styrene, vinyl esters, vinyl ethers, N-vinyl-2-pyrrolidone, (meth)acrylamide, vinyl naphthalene, alkylated vinyl 10 naphthalenes, alkoxy vinyl naphthalenes, N-substituted (meth)acrylamide, octyl (meth)acrylate, nonylphenol ethoxylate (meth)acrylate, N-vinyl pyrrolidone, isononyl (meth)acrylate, isobornyl (meth)acrylate, 2-(2-ethoxyethoxy)ethyl (meth)acrylate, 2-ethylhexyl (meth)acrylate, beta-carboxyethyl (meth)acrylate, isobutyl (meth)acrylate, cycloaliphatic epoxide, alpha-epoxide, 2-hydroxyethyl (meth)acrylate, 15 (meth)acrylonitrile, maleic anhydride, itaconic acid, isodecyl (meth)acrylate, lauryl (dodecyl) (meth)acrylate, steryl (octadecyl) (meth)acrylate, behenyl (meth)acrylate, n-butyl (meth)acrylate, methyl (meth)acrylate, ethyl (meth)acrylate, hexyl (meth)acrylate, (meth)acrylic acid, N-vinylcaprolactam, steryl (meth)acrylate, hydroxy functional 20 caprolactone ester (meth)acrylate, isoctyl (meth)acrylate, hydroxyethyl (meth)acrylate, hydroxymethyl (meth)acrylate, hydroxypropyl (meth)acrylate, hydroxyisopropyl (meth)acrylate, hydroxybutyl (meth)acrylate, hydroxyisobutyl (meth)acrylate, tetrahydrofurfuryl (meth)acrylate, isobornyl (meth)acrylate, glycidyl (meth)acrylate vinyl acetate, combinations of these, and the like.

Preferred copolymers of the present invention may be formulated with one or 25 more radiation curable monomers or combinations thereof that help the free radically polymerizable compositions and/or resultant cured compositions to satisfy one or more desirable performance criteria. For example, in order to promote hardness and abrasion resistance, a formulator may incorporate one or more free radically polymerizable monomer(s) (hereinafter "high T_g component") whose presence causes the polymerized 30 material, or a portion thereof, to have a higher glass transition temperature, T_g, as compared to an otherwise identical material lacking such high T_g component. Preferred

monomeric constituents of the high T_g component generally include monomers whose homopolymers have a T_g of at least about 50°C, preferably at least about 60°C, and more preferably at least about 75°C in the cured state.

An exemplary class of radiation curable monomers that tend to have relatively high T_g characteristics suitable for incorporation into the high T_g component generally comprise at least one radiation curable (meth)acrylate moiety and at least one nonaromatic, alicyclic and/or nonaromatic heterocyclic moiety. Isobornyl (meth)acrylate is a specific example of one such monomer. A cured, homopolymer film formed from isobornyl acrylate, for instance, has a T_g of 110°C. The monomer itself has a molecular weight of 222 g/mole, exists as a clear liquid at room temperature, has a viscosity of 9 centipoise at 25°C, and has a surface tension of 31.7 dynes/cm at 25°C. Additionally, 1,6-Hexanediol di(meth)acrylate is another example of a monomer with high T_g characteristics.

Trimethyl cyclohexyl methacrylate (TCHMA) is another example of a high T_g monomer useful in the practice of the present invention. TCHMA has a T_g of 125°C and tends to be soluble in oleophilic solvents. Consequently, TCHMA is easily incorporated into S material. However, if used in limited amounts so as not to unduly impair the insolubility characteristics of D material, some TCHMA may also be incorporated into D the material.

In a particularly preferred embodiment of the present invention, the S portion of the copolymer has a glass transition temperature calculated using the Fox equation (excluding grafting site components) of at least about 90°C, and more preferably has a glass transition temperature calculated using the Fox equation (excluding grafting site components) of from about 100°C to about 130°C. Preferably, at least about 75%, and more preferably at least about 90%, of the S portion (excluding grafting site components) is derived from ingredients selected from the group consisting of trimethyl cyclohexyl methacrylate; t-butyl methacrylate; n-butyl methacrylate; isobornyl (meth)acrylate; 1,6-Hexanediol di(meth)acrylate and combinations thereof. Toners using copolymers having the above described S portion characteristics exhibit particularly superior performance properties in image quality and transfer as described herein.

Nitrile functionality may be advantageously incorporated into the copolymer for a variety of reasons, including improved durability, enhanced compatibility with optional visual enhancement additive(s), e.g., colorant particles, and the like. In order to provide a copolymer having pendant nitrile groups, one or more nitrile functional monomers can be used. Representative examples of such monomers include (meth)acrylonitrile, β -cyanoethyl-(meth)acrylate, 2-cyanoethoxyethyl (meth)acrylate, p-cyanostyrene, p-(cyanomethyl)styrene, N-vinylpyrrolidinone, and the like.

In order to provide a copolymer having pendant hydroxyl groups, one or more hydroxyl functional monomers can be used. Pendant hydroxyl groups of the copolymer not only facilitate dispersion and interaction with the pigments in the formulation, but also promote solubility, cure, reactivity with other reactants, and compatibility with other reactants. The hydroxyl groups can be primary, secondary, or tertiary, although primary and secondary hydroxyl groups are preferred. When used, hydroxy functional monomers constitute from about 0.5 to 30, more preferably 1 to about 25 weight percent of the monomers used to formulate the copolymer, subject to preferred weight ranges for graft copolymers noted below.

Representative examples of suitable hydroxyl functional monomers include an ester of an α , β -unsaturated carboxylic acid with a diol, e.g., 2-hydroxyethyl (meth)acrylate, or 2-hydroxypropyl (meth)acrylate; 1,3-dihydroxypropyl-2-(meth)acrylate; 2,3-dihydroxypropyl-1-(meth)acrylate; an adduct of an α , β -unsaturated carboxylic acid with caprolactone; an alkanol vinyl ether such as 2-hydroxyethyl vinyl ether; 4-vinylbenzyl alcohol; allyl alcohol; p-methylol styrene; or the like.

Polymerizable crystallizable compound(s) (PCC's), e.g. crystalline monomer(s), also may be advantageously incorporated into the copolymer in order to improve blocking resistance between printed receptors and to reduce offset during fusing. Polymerizable crystallizable compounds are incorporated into the copolymer by chemical incorporation, e.g., polymerization or copolymerization. The term "crystalline monomer" refers to a monomer whose homopolymeric analog is capable of independently and reversibly crystallizing at or above room temperature (e.g., 22°C).

In these embodiments, the resulting toner particles can exhibit improved blocking resistance between printed receptors and reduced offset during fusing. If used, one or

more of these crystalline monomers may be incorporated into the S and/or D material, but preferably is incorporated into the D material. Suitable crystalline monomers include alkyl(meth)acrylates where the alkyl chain contains more than 13 carbon atoms (e.g. tetradecyl(meth)acrylate, pentadecyl(meth)acrylate, hexadecyl(meth)acrylate,
5 heptadecyl(meth)acrylate, octadecyl(meth)acrylate, etc). Other suitable crystalline monomers whose homopolymers have melting points above 22°C include aryl acrylates and methacrylates; high molecular weight alpha olefins; linear or branched long chain alkyl vinyl ethers or vinyl esters; long chain alkyl isocyanates; unsaturated long chain polyesters, polysiloxanes and polysilanes; polymerizable natural waxes with melting
10 points above 22°C; polymerizable synthetic waxes with melting points above 22°C; and other similar type materials known to those skilled in the art. As described herein, incorporation of crystalline monomers in the copolymer provides surprising benefits to the resulting dry toner particles.

It will be understood by those skilled in the art that blocking resistance can be
15 observed at temperatures above room temperature but below the crystallization temperature of the polymer or copolymer portion incorporating the crystalline monomers or other polymerizable crystallizable compound. Improved blocking resistance is observed when the crystalline monomer is a major component of the S material, preferably greater than or equal to 45%, more preferably greater than or equal to 75%,
20 most preferably greater than or equal to 90% of the S material incorporated into the copolymer.

Many crystalline monomers tend to be soluble in oleophilic solvents commonly used as liquid carrier material(s) in an organosol. Thus, crystalline monomer is relatively easily incorporated into S material without impacting desired solubility characteristics.
25 However, if too much of such crystalline monomer were to be incorporated into D material, the resultant D material may tend to be too soluble in the organosol. Yet, so long as the amount of soluble, crystalline monomer in the D material is limited, some amount of crystalline monomer may be advantageously incorporated into the D material without unduly impacting the desired insolubility characteristics. Thus, when present in
30 the D material, the crystalline monomer is preferably provided in an amount of up to

about 30%, more preferably up to about 20%, most preferably up to about 5% to 10% of the total D material incorporated into the copolymer.

When crystalline monomers or PCC's are chemically incorporated into the S material, suitable co-polymerizable compounds that can be used in combination with the PCC include monomers such as other PCC's, 2-ethylhexyl acrylate, 2-ethylhexyl (methacrylate), lauryl acrylate, lauryl methacrylate, octadecyl acrylate, octadecyl(methacrylate), isobornyl acrylate, isobornyl (methacrylate), hydroxy(ethylmethacrylate), other acrylates and methacrylates, combinations of these and the like.

It is also advantageous to incorporate monomers into the copolymer that provide polymerized portions that are inherently triboelectrically charged. When used, it is preferred to incorporate such materials into the S material, as this material tends to be more solvated by the liquid carrier and is therefore located towards the outside surface or shell of the resultant triboelectrically charged toner particles. Monomers that provide

polymer portions with positive and/or negative triboelectric charges may be used in amounts effective to produce the desired inherent triboelectric charge characteristics. For instance, butyl methacrylate generally tends to provide a more positive (less negative) triboelectric charge while styrene tends to provide a more negative (less positive) triboelectric charge, particularly when used in combination with other monomers.

Multifunctional free radically reactive materials may also be used to enhance one or more properties of the resultant toner particles, including crosslink density, hardness, tackiness, mar resistance, or the like. Examples of such higher functional, monomers include ethylene glycol di(meth)acrylate, hexanediol di(meth)acrylate, triethylene glycol di(meth)acrylate, tetraethylene glycol di(meth)acrylate, trimethylolpropane

tri(meth)acrylate, ethoxylated trimethylolpropane tri(meth)acrylate, glycerol tri(meth)acrylate, pentaerythritol tri(meth)acrylate, pentaerythritol tetra(meth)acrylate, and neopentyl glycol di(meth)acrylate, divinyl benzene, combinations of these, and the like.

Suitable free radically reactive oligomer and/or polymeric materials for use in the present invention include, but are not limited to, (meth)acrylated urethanes (i.e., urethane (meth)acrylates), (meth)acrylated epoxies (i.e., epoxy (meth)acrylates), (meth)acrylated

polyesters (i.e., polyester (meth)acrylates), (meth)acrylated (meth)acrylics, (meth)acrylated silicones, (meth)acrylated polyethers (i.e., polyether (meth)acrylates), vinyl (meth)acrylates, and (meth)acrylated oils.

Reactive colorants to be incorporated in the amphipathic copolymers of the present invention may be any chromophore compound having functional groups that will react with functional groups on components forming the amphipathic copolymer to form a urethane, urea or amide linkage. For example, when the functional group on components forming the amphipathic copolymer is an isocyanate functionality, the chromophore compound has functional groups selected from hydroxyl, amino and carboxyl functionality. Similarly, when the functional group on components forming the amphipathic copolymer is selected from hydroxyl, amino and carboxyl functionality, the chromophore compound has an isocyanate functionality. Examples of such chromophore compounds are known in the art, and include those disclosed in United States Patent Nos 4,614,521 to Niwa, et. al.; 4,775,748 to Kluger et al.; 4,985,546 to Miley, et al.; 5,082,938 to Kluger et al.; 5,290,921 to Moody, et al.; 5,919,846 to Batlaw, et al.; and 6,077,927 to Stephens, et al.

Copolymers of the present invention can be prepared by free-radical polymerization methods known in the art, including but not limited to bulk, solution, and dispersion polymerization methods. The resultant copolymers may have a variety of structures including linear, branched, three dimensionally networked, graft-structured, combinations thereof, and the like. A preferred embodiment is a graft copolymer comprising one or more oligomeric and/or polymeric arms attached to an oligomeric or polymeric backbone. In graft copolymer embodiments, the S portion or D portion materials, as the case may be, may be incorporated into the arms and/or the backbone.

Any number of reactions known to those skilled in the art may be used to prepare a free radically polymerized copolymer having a graft structure. Common grafting methods include random grafting of polyfunctional free radicals; copolymerization of monomers with macromonomers; ring-opening polymerizations of cyclic ethers, esters, amides or acetals; epoxidations; reactions of hydroxyl or amino chain transfer agents with terminally-unsaturated end groups; esterification reactions (i.e., glycidyl methacrylate

undergoes tertiary-amine catalyzed esterification with methacrylic acid); and condensation polymerization.

Representative methods of forming graft copolymers are described in U.S. Pat. Nos. 6,255,363; 6,136,490; and 5,384,226; and Japanese Published Patent Document No.

5 05-119529, incorporated herein by reference. Representative examples of grafting methods are also described in sections 3.7 and 3.8 of "Dispersion Polymerization in Organic Media," K.E.J. Barrett, ed., (John Wiley; New York, 1975) pp. 79-106, also incorporated herein by reference.

Representative examples of grafting methods also may use an anchoring group to facilitate anchoring. The function of the anchoring group is to provide a covalently bonded link between the core part of the copolymer (the D material) and the soluble shell component (the S material). Suitable monomers containing anchoring groups include: adducts of alkenylazlactone comonomers with an unsaturated nucleophile containing hydroxy, amino, or mercaptan groups, such as 2-hydroxyethylmethacrylate, 3-hydroxypropylmethacrylate, 2-hydroxyethylacrylate, pentaerythritol triacrylate, 4-hydroxybutylvinylether, 9-octadecen-1-ol, cinnamyl alcohol, allyl mercaptan, methallylamine; and azlactones, such as 2-alkenyl-4,4-dialkylazlactone.

In one aspect of the present invention a method of making an amphipathic copolymer comprising at least one covalently bonded chromophore is provided. In this method, a plurality of free radically polymerizable monomers is provided wherein at least one of the monomers comprises a first reactive functionality. These monomers are free radically polymerized in a solvent to form a first reactive functional polymer, wherein the monomers and the first reactive functional polymer are soluble in the solvent. A compound having a second reactive functionality that is reactive with the first reactive functionality and also contains free radically polymerizable functionality is reacted with the first reactive functional polymer under conditions such that at least a portion of the second reactive functionality of the compound reacts with at least a portion of the first reactive functionality of the polymer to form one or more linkages by which the compound is linked to the polymer. The resulting polymer is an S material portion polymer with pendant free radically polymerizable functionality.

A composition comprising (i) the S material portion polymer with pendant free radically polymerizable functionality described above, (ii) one or more free radically polymerizable monomers, (iii) a chromophore comprising a third reactive functionality, and (iv) liquid carrier in which polymeric material derived from ingredients comprising the one or more additional monomers of ingredient (ii) is insoluble is then polymerized.

5 At least one of the ingredients (i) and (ii) above comprises a fourth reactive functionality that is available for reaction. In the above compositions, one of the third and fourth reactive functionalities is an isocyanate functionality, and the other of the third and fourth reactive functionalities is selected from the group consisting of hydroxyl, amino,

10 carboxyl or mixtures thereof. The copolymerizing occurs under conditions effective to form an amphipathic copolymer having S and D portions and a chromophore covalently bonded thereto via a urethane, urea or amide linkage. Preferably, one of the first and second reactive functionality is selected from hydroxyl, amino, and carboxyl functionalities, and mixtures thereof, and the other of the first and second reactive

15 functionalities is selected from isocyanate and epoxy functionalities.

The chromophore may be covalently bonded to the S portion of the amphipathic copolymer, the D portion of the amphipathic copolymer, or both the S and D portions.

The preferred methodology described below accomplishes grafting via attaching an ethylenically-unsaturated isocyanate (e.g. dimethyl-m-isopropenyl benzylisocyanate, TMI, available from CYTEC Industries, West Paterson, NJ; or isocyanatoethyl methacrylate, also known as IEM) to hydroxyl groups in order to provide free radically reactive anchoring groups.

A preferred method of forming a graft copolymer of the present invention involves three reaction steps that are carried out in a suitable substantially nonaqueous liquid carrier in which resultant S material is soluble while D material is dispersed or insoluble. In a first preferred step, a hydroxyl functional, free radically polymerized oligomer or polymer is formed from one or more monomers, wherein at least one of the monomers has pendant hydroxyl functionality. Preferably, the hydroxyl functional monomer constitutes about 1 to about 30, preferably about 2 to about 10 percent, most 25 preferably 3 to about 5 percent by weight of the monomers used to form the oligomer or polymer of this first step. This first step is preferably carried out via solution

polymerization in a substantially nonaqueous solvent in which the monomers and the resultant polymer are soluble. For instance, using the Hildebrand solubility data in Table 1, monomers such as octadecyl methacrylate, octadecyl acrylate, lauryl acrylate, and lauryl methacrylate are suitable for this first reaction step when using an oleophilic solvent such as heptane or the like.

In a second reaction step, all or a portion of the hydroxyl groups of the soluble polymer are catalytically reacted with an ethylenically unsaturated aliphatic isocyanate (e.g. meta-isopropenylidemethylbenzyl isocyanate commonly known as TMI or isocyanatoethyl methacrylate, commonly known as IEM) to form pendant free radically polymerizable functionality which is attached to the oligomer or polymer via a polyurethane linkage. This reaction can be carried out in the same solvent, and hence the same reaction vessel, as the first step. The resultant double-bond functionalized polymer generally remains soluble in the reaction solvent and constitutes the S portion material of the resultant copolymer, which ultimately will constitute at least a portion of the solvatable portion of the resultant triboelectrically charged particles. When the chromophore is to be located at the S portion of the amphipathic copolymer, preferably there are available NCO groups during or after this polymerization process for reaction with hydroxyl functionality on a chromophore compound.

The resultant free radically reactive functionality provides grafting sites for attaching D material and optionally additional S material to the polymer. In a third step, these grafting site(s) are used to covalently graft such material to the polymer via reaction with one or more free radically reactive monomers, oligomers, and or polymers that are initially soluble in the solvent, but then become insoluble as the molecular weight of the graft copolymer increases. For instance, using the Hildebrand solubility parameters in Table 1, monomers such as e.g. methyl (meth)acrylate, ethyl (meth)acrylate, t-butyl methacrylate and styrene are suitable for this third reaction step when using an oleophilic solvent such as heptane or the like. When the chromophore is to be located at the D portion of the amphipathic copolymer, preferably there are available NCO groups during or after this polymerization process for reaction with hydroxyl functionality on a chromophore compound.

The product of the third reaction step is generally an organosol comprising the resultant copolymer dispersed in the reaction solvent, which constitutes a substantially nonaqueous liquid carrier for the organosol. At this stage, it is believed that the copolymer tends to exist in the liquid carrier as discrete, monodisperse particles having dispersed (e.g., substantially insoluble, phase separated) portion(s) and solvated (e.g., substantially soluble) portion(s). As such, the solvated portion(s) help to sterically-stabilize the dispersion of the particles in the liquid carrier. It can be appreciated that the copolymer is thus advantageously formed in the liquid carrier in situ.

Before further processing, the copolymer particles may remain in the reaction solvent. Alternatively, the particles may be transferred in any suitable way into fresh solvent that is the same or different so long as the copolymer has solvated and dispersed phases in the fresh solvent. In either case, the resulting chromophore-containing organosol may optionally additionally incorporate visible enhancement additives by preferably mixing the organosol with at least one visual enhancement additive.

15 Optionally, one or more other desired ingredients also can be mixed into the organosol before and/or after combination with the visual enhancement particles. During such combination, it is believed that ingredients comprising the visual enhancement additive and the copolymer will tend to self-assemble into composite particles having a structure wherein the dispersible phase portions generally tend to associate with the visual enhancement additive particles (for example, by physically and/or chemically interacting with the surface of the particles), while the solvatable phase portions help promote dispersion in the carrier. The dispersion is then dried to the desired degree to provide composite particles that have dry toner functionality.

20

The manner in which the dispersion is dried, when preparing dry toner compositions, may impact the degree to which the resultant toner particles may be agglomerated and/or aggregated. In preferred modes of practice, the particles are dried while fluidized, aspirated, suspended, or entrained (collectively "fluidized") in a carrier gas to minimize aggregation and/or agglomeration of the dry toner particles as the particles dry. In practical effect, the fluidized particles are dried while in a low density condition. This minimizes interparticle collisions, allowing particles to dry in relative isolation from other particles. Such fluidizing may be achieved using vibration energy,

electrostatic energy, a moving gas, combinations of these, and the like. The carrier gas may comprise one or more gases that may be generally inert (e.g. nitrogen, air, carbon dioxide, argon, or the like). Alternatively, the carrier gas may include one or more reactive species. For instance, an oxidizing and/or reducing species may be used if desired. Advantageously, the product of fluidized drying constitutes free flowing dry toner particles with a narrow particle size distribution.

- As one example of using a fluidized bed dryer, the liquid toners may be filtered or centrifuged to form a wet cake. The wet filter cake may be placed into the conical drying chamber of a fluid bed dryer (such as that available from Niro Aeromatic, Niro Corp., 10 Hudson, WI). Ambient air at about 35-50°C, or preferably lower than the T_g of the copolymer, may be passed through the chamber (from bottom to top) with a flow rate sufficient to loft any dried powder and to keep the powder airborne inside the vessel (i.e., a fluidized powder bed). The air may be heated or otherwise pretreated. Bag filters in the vessel allow the air to leave the drying vessel while keeping the powder contained.
- 15 Any toner that accumulates on the filter bags may be blown down by a periodic reverse air flow through the filters. Samples may be dried anywhere from 10-20 minutes to several hours, depending on the nature of the solvent (e.g. boiling point), the initial solvent content, and the drying conditions.

Advantageously, the S material of the copolymer serves as a graft stabilizer, 20 chemically bonded steric stabilizer, or internal dispersant for the toner particles in the fluidized state. Consequently, although separate dispersant material could be used to help mix the dry toner ingredients together, the use of a separate dispersant material is not needed, or even desirable, in preferred embodiments. Separate dispersants are less desirable as these tend to be humidity sensitive, and may migrate from the toner particles 25 during printing. Dry toner particles incorporating separate dispersant material may tend to have charging characteristics that vary with humidity changes. By avoiding separate dispersant material, it is believed that preferred embodiments of the present invention would show more stable charging characteristics with changes in humidity.

The optional visual enhancement additive(s) generally may include any one or 30 more fluid and/or particulate materials that provide a desired visual effect when toner particles incorporating such materials are printed onto a receptor. Examples include one

or more colorants, fluorescent materials, pearlescent materials, iridescent materials, metallic materials, flip-flop pigments, silica, polymeric beads, reflective and non-reflective glass beads, mica, combinations of these, and the like. The amount of visual enhancement additive incorporated into the toner particles may vary over a wide range.

- 5 In representative embodiments, a suitable weight ratio of copolymer to visual enhancement additive is from 1/1 to 20/1, preferably from 2/1 to 10/1 and most preferably from 4/1 to 8/1.

Useful colorants to be used as optional additional visual enhancement additives are well known in the art and include materials listed in the Colour Index, as published by the Society of Dyers and Colourists (Bradford, England), including dyes, stains, and pigments. Preferred colorants are pigments which may be combined with ingredients comprising the copolymer to interact with the D portion of the copolymer to form dry toner particles with structure as described herein, are at least nominally insoluble in and nonreactive with the carrier liquid, and are useful and effective in making visible the latent electrostatic image. It is understood that the optional visual enhancement additive(s) may also interact with each other physically and/or chemically, forming aggregations and/or agglomerates of visual enhancement additives that also interact with the D portion of the copolymer. Examples of suitable colorants include: phthalocyanine blue (C.I. Pigment Blue 15:1, 15:2, 15:3 and 15:4), monoarylide yellow (C.I. Pigment Yellow 1, 3, 65, 73 and 74), diarylide yellow (C.I. Pigment Yellow 12, 13, 14, 17 and 83), arylamide (Hansa) yellow (C.I. Pigment Yellow 10, 97, 105 and 111), isoindoline yellow (C.I. Pigment Yellow 138), azo red (C.I. Pigment Red 3, 17, 22, 23, 38, 48:1, 48:2, 52:1, and 52:179), quinacridone magenta (C.I. Pigment Red 122, 202 and 209), laked rhodamine magenta (C.I. Pigment Red 81:1, 81:2, 81:3, and 81:4), and black pigments such as finely divided carbon (Cabot Monarch 120, Cabot Regal 300R, Cabot Regal 350R, Vulcan X72, and Aztech ED 8200), and the like.

In addition to the visual enhancement additive, other additives optionally may be formulated into the triboelectrically charged particle formulation. A particularly preferred additive comprises at least one charge control additive (charge control agent, CCA). The charge control additive, also known as a charge director, helps to provide uniform charge polarity of the toner particles. The charge director may be incorporated

into the toner particles using a variety of methods such as, copolymerizing a suitable monomer with the other monomers used to form the copolymer, chemically reacting the charge director with the toner particle, chemically or physically adsorbing the charge director onto the toner particle (resin or pigment), or chelating the charge director to a 5 functional group incorporated into the toner particle. A preferred method is via a functional group built into the S material of the copolymer.

It is preferable to use a triboelectric charge control additive that may be included as a separate ingredient and/or included as one or more functional moiety(ies) of S and/or D material incorporated into the amphipathic copolymer. The triboelectric charge 10 control additive is used to enhance the chargeability of the toner. The triboelectric charge control agent may have either a negative or a positive electric charge. As representative examples of the triboelectric charge control additive, there can be mentioned nigrosine NO1 (produced by Orient Chemical Co.), nigrosine EX (produced by Orient Chemical Co.), Aizen Spilon black TRH (produced by Hodogaya Chemical Co.), T-77 (produced 15 by Hodogaya Chemical Co.), Bontron S-34 (produced by Orient Chemical Co.), and Bontron E-84 (produced by Orient Chemical Co.). The amount of the triboelectric charge control additive, based on 100 parts by weight of the toner solids, is generally 0.01 to 10 parts by weight, preferably 0.1 to 5 parts by weight.

Other additives may also be added to the formulation in accordance with 20 conventional practices. These include one or more of UV stabilizers, mold inhibitors, bactericides, fungicides, antistatic agents, gloss modifying agents, other polymer or oligomer material, antioxidants, anticaking agents such as silane or silicone-modified silica particles (typically 5 to 50 nm particle size), combinations of these, and the like.

The particle size of the resultant triboelectrically charged toner particles may 25 impact the imaging, fusing, resolution, and transfer characteristics of the toner incorporating such particles. Preferably, the volume mean particle diameter (determined by laser diffraction light scattering) of the toner particles is in the range of about 0.5 to about 30.0 microns, more preferably in the range of about 1 to about 15 microns, most preferably in the range of about 3 to about 10 microns.

30 In electrophotographic and electrographic processes, an electrostatic image is formed on the surface of a photoreceptive element or dielectric element, respectively. The

photoreceptive element or dielectric element may be an intermediate transfer drum or belt or the substrate for the final toned image itself, as described by Schmidt, S. P. and Larson, J. R. in *Handbook of Imaging Materials* Diamond, A. S., Ed: Marcel Dekker: New York; Chapter 6, pp 227-252, and U.S. Pat. Nos. 4,728,983; 4,321,404; and
5 4,268,598.

In electrography, a latent image is typically formed by (1) placing a charge image onto the dielectric element (typically the receiving substrate) in selected areas of the element with an electrostatic writing stylus or its equivalent to form a charge image, (2) applying toner to the charge image, and (3) fixing the toned image. An example of this
10 type of process is described in U.S. Pat. No. 5,262,259. Images formed by the present invention may be of a single color or a plurality of colors. Multicolor images can be prepared by repetition of the charging and toner application steps.

In electrophotography, the electrostatic image is typically formed on a drum or belt coated with a photoreceptive element by (1) uniformly charging the photoreceptive
15 element with an applied voltage, (2) exposing and discharging portions of the photoreceptive element with a radiation source to form a latent image, (3) applying a toner to the latent image to form a toned image, and (4) transferring the toned image through one or more steps to a final receptor sheet. In some applications, it is sometimes desirable to fix the toned image using a heated pressure roller or other fixing methods
20 known in the art.

While the electrostatic charge of either the toner particles or photoreceptive element may be either positive or negative, electrophotography as employed in the present invention is preferably carried out by dissipating charge on a positively charged photoreceptive element. A positively-charged toner is then applied to the regions in
25 which the positive charge was dissipated using a dry toner development technique.

The substrate for receiving the image from the photoreceptive element can be any commonly used receptor material, such as paper, coated paper, polymeric films and primed or coated polymeric films. Polymeric films include polyesters and coated polyesters, polyolefins such as polyethylene or polypropylene, plasticized and
30 compounded polyvinyl chloride (PVC), acrylics, polyurethanes, polyethylene/acrylic acid.

copolymer, and polyvinyl butyral. The polymer film may be coated or primed, e.g. to promote toner adhesion.

These and other aspects of the present invention are demonstrated in the illustrative examples that follow.

5

EXAMPLES

Test Methods and Apparatus

In the following examples, percent solids of the copolymer solutions and the
10 organosol and ink dispersions were determined gravimetrically using the Halogen Lamp Drying Method using a halogen lamp drying oven attachment to a precision analytical balance (Mettler Instruments, Inc., Highstown, N.J.). Approximately two grams of sample were used in each determination of percent solids using this sample dry down method.

15 In the practice of the invention, molecular weight is normally expressed in terms of the weight average molecular weight, while molecular weight polydispersity is given by the ratio of the weight average molecular weight to the number average molecular weight. Molecular weight parameters were determined with gel permeation chromatography (GPC) using tetrahydrofuran as the carrier solvent. Absolute weight
20 average molecular weight were determined using a Dawn DSP-F light scattering detector (Wyatt Technology Corp., Santa Barbara, Calif.), while polydispersity was evaluated by ratioing the measured weight average molecular weight to a value of number average molecular weight determined with an Optilab 903 differential refractometer detector (Wyatt Technology Corp., Santa Barbara, Calif.).

25 Organosol and toner particle size distributions were determined by a Laser Diffraction Method using a Horiba LA-900 laser diffraction particle size analyzer (Horiba Instruments, Inc., Irvine, Calif.). Samples were diluted approximately 1/500 by volume and sonicated for one minute at 150 watts and 20 kHz prior to measurement. Particle size was expressed as both a number mean diameter (D_n) and a volume mean
30 diameter (D_v) and in order to provide an indication of both the fundamental (primary) particle size and the presence of aggregates or agglomerates.

The liquid toner conductivity (bulk conductivity, k_b) was determined at approximately 18 Hz using a Scientifica Model 627 conductivity meter (Scientifica Instruments, Inc., Princeton, N.J.). In addition, the free (liquid dispersant) phase conductivity (k_f) in the absence of toner particles was also determined. Toner particles 5 were removed from the liquid medium by centrifugation at 5°C for 1-2 hours at 6,000 rpm (6,110 relative centrifugal force) in a Jouan MR1822 centrifuge (Winchester, VA). The supernatant liquid was then carefully decanted, and the conductivity of this liquid was measured using a Scientifica Model 627 conductance meter. The percentage of free 10 phase conductivity relative to the bulk toner conductivity was then determined as 100% (k_f/k_b).

Toner particle electrophoretic mobility (dynamic mobility) was measured using a Matec MBS-8000 Electrokinetic Sonic Amplitude Analyzer (Matec Applied Sciences, Inc., Hopkinton, MA). Unlike electrokinetic measurements based upon microelectrophoresis, the MBS-8000 instrument has the advantage of requiring no dilution of the 15 toner sample in order to obtain the mobility value. Thus, it is possible to measure toner particle dynamic mobility at solids concentrations actually preferred in printing. The MBS-8000 measures the response of charged particles to high frequency (1.2 MHz) alternating (AC) electric fields. In a high frequency AC electric field, the relative motion between charged toner particles and the surrounding dispersion medium (including 20 counter-ions) generates an ultrasonic wave at the same frequency of the applied electric field. The amplitude of this ultrasonic wave at 1.2 MHz can be measured using a piezoelectric quartz transducer; this electrokinetic sonic amplitude (ESA) is directly proportional to the low field AC electrophoretic mobility of the particles. The particle zeta potential can then be computed by the instrument from the measured dynamic 25 mobility and the known toner particle size, liquid dispersant viscosity, and liquid dielectric constant.

The charge per mass measurement (Q/M) was measured using an apparatus that consists of a conductive metal plate, a glass plate coated with Indium Tin Oxide (ITO), a high voltage power supply, an electrometer, and a personal computer (PC) for data 30 acquisition. A 1% solution of ink was placed between the conductive plate and the ITO coated glass plate. An electrical potential of known polarity and magnitude was applied

between the ITO coated glass plate and the metal plate, generating a current flow between the plates and through wires connected to the high voltage power supply. The electrical current was measured 100 times a second for 20 seconds and recorded using the PC. The applied potential causes the charged toner particles to migrate towards the plate 5 (electrode) having opposite polarity to that of the charged toner particles. By controlling the polarity of the voltage applied to the ITO coated glass plate, the toner particles may be made to migrate to that plate.

The ITO coated glass plate was removed from the apparatus and placed in an oven for approximately 30 minutes at 50°C to dry the plated ink completely. After 10 drying, the ITO coated glass plate containing the dried ink film was weighed. The ink was then removed from the ITO coated glass plate using a cloth wipe impregnated with Norpar™ 12, and the clean ITO glass plate was weighed again. The difference in mass between the dry ink coated glass plate and the clean glass plate is taken as the mass of ink particles (m) deposited during the 20 second plating time. The electrical current values 15 were used to obtain the total charge carried by the toner particles (Q) over the 20 seconds of plating time by integrating the area under a plot of current vs. time using a curve-fitting program (e.g. TableCurve 2D from Systat Software Inc.). The charge per mass (Q/m) was then determined by dividing the total charge carried by the toner particles by the dry plated ink mass.

20 In the following examples, toner was printed onto final image receptors using the following methodology (referred to in the Examples as the Liquid Electrophotographic Printing Method):

A light sensitive temporary image receptor (organic photoreceptor or “OPC”) was charged with a uniform positive charge of approximately 850 volts. The positively 25 charged surface of the OPC was image-wise irradiated with a scanning infrared laser module in order to reduce the charge wherever the laser struck the surface. Typical charge-reduced values were between 50 volts and 100 volts.

A developer apparatus was then utilized to apply the toner particles to the OPC surface. The developer apparatus included the following elements: a conductive rubber 30 developer roll in contact with the OPC, liquid toner, a conductive deposition roll, an insulative foam cleaning roll in contact with developer roll surface, and a conductive

skiving blade (skive) in contact with the developer roll. The contact area between the developer roll and the OPC is referred to as the "developing nip." The developer roll and conductive deposition roll were both partially suspended in the liquid toner. The developer roll delivered liquid toner to the OPC surface, while the conductive deposition 5 roll was positioned with its roll axis parallel to the developer roll axis and its surface arranged to be approximately 150 microns from the surface of the developer roll, thereby forming a deposition gap.

During development, toner was initially transferred to the developer roll surface by applying a voltage of approximately 500 volts to the conductive developer roll and 10 applying a voltage of 600 volts to the deposition roll. This created a 100-volt potential between the developer roll and the deposition roll so that in the deposition gap, toner particles (which were positively charged) migrated to the surface of the developer roll and remained there as the developer roll surface exited from the liquid toner into the air.

The conductive metal skive was biased to at least 600 volts (or more) and skived 15 liquid toner from the surface of the developer roll without scraping off the toner layer that was deposited in the deposition gap. The developer roll surface at this stage contained a uniformly thick layer of toner at approximately 25% solids. As this toner layer passed through the developing nip, toner was transferred from the developer roll surface to the OPC surface in all the discharged areas of the OPC (the charge image), since the toner 20 particles were positively charged. At the exit of the developing nip, the OPC contained a toner image and the developer roll contained a negative of that toner image which was subsequently cleaned from the developer roll surface by encountering the rotating foam cleaning roll.

The developed latent image (toned image) on the photoreceptor was subsequently 25 transferred to the final image receptor without film formation of the toner on the OPC. Transfer was effected either directly to the final image receptor, or indirectly using an electrostatically-assisted offset transfer to an Intermediate Transfer Belt (ITB), with subsequent electrostatically-assisted offset transfer to the final image receptor. Smooth, clay coated papers were preferred final image receptors for direct transfer of a non-film 30 formed toner from the photoreceptor, while plain, uncoated 20 pound bond paper was a preferred final image receptor for offset transfer using an electrostatic assist.

Electrostatically-assisted transfer of non film-formed toner was most effective when the transfer potential (potential difference between the toner on the OPC and the paper back-up roller for direct transfer; or potential difference between the toner on the OPC and the ITB for offset transfer) was maintained in the range of 200-1000 V or 800-2000 V,
5 respectively.

Materials

- LMA: lauryl methacrylate
10 HEMA: 2-hydroxyethyl methacrylate
TMI: dimethyl-m-isopropenyl benzyl isocyanate
EA: ethyl acrylate
EMA: ethyl methacrylate
V-601: initiator, dimethyl 2, 2'-azobisisobutyrate
15 DBTDL: catalyst, dibutyl tin dilaurate.

Examples 1: Preparation of Graft Copolymer Stabilizers

Example 1

20 A 5000 ml 3-neck round flask equipped with a condenser, a thermocouple connected to a digital temperature controller, a nitrogen inlet tube connected to a source of dry nitrogen and a magnetic stirrer, was charged with a mixture of 2557 g of NorparTM 12, 849 g of LMA, 26.8 g of 98% HEMA and 13.13 g of V-601. While stirring the mixture, the reaction flask was purged with dry nitrogen for 30 minutes at flow rate of
25 approximately 2 liters/minute. A hollow glass stopper was then inserted into the open end of the condenser and the nitrogen flow rate was reduced to approximately 0.5 liters/minute. The mixture was heated to 70° C for 16 hours. The conversion was quantitative.

30 The mixture was heated to 90° C and held at that temperature for 1 hour to destroy any residual V-601, then was cooled back to 70° C. The nitrogen inlet tube was then removed, and 13.6 g of 95% DBTDL were added to the mixture, followed by 41.1 g of

TMI. The TMI was added drop wise over the course of approximately 5 minutes while stirring the reaction mixture. The nitrogen inlet tube was replaced, the hollow glass stopper in the condenser was removed, and the reaction flask was purged with dry nitrogen for 30 minutes at a flow rate of approximately 2 liters/minute. The hollow glass
5 stopper was reinserted into the open end of the condenser and the nitrogen flow rate was reduced to approximately 0.5 liters/minute. The mixture was allowed to react at 70°C for 6 hours, at which time the conversion was quantitative.

The mixture was then cooled to room temperature. The cooled mixture was viscous, transparent solution, containing no visible insoluble matter.

10 The percent solids of the liquid mixture was determined to be 25.98% using the Halogen Drying Method described above. Subsequent determination of molecular weight was made using the GPC method described above; the copolymer had a M_w 191,550 of Da and M_w/M_n of 2.5 based upon two independent measurements. The product is a copolymer of LMA and HEMA containing random side chains of TMI and is
15 designed herein as LMA/HEMA-TMI (97/3-4.7% w/w) and is suitable for making an organosol.

Examples 2-5: Preparation of Organosols by Incorporating Reactint™ Urethane Colorants.

20

Example 2 (comparative)

This is a comparative example using the graft stabilizer in Example 1 to prepare an organosol which containing no Reactint™ Urethane Colorants. A 8 ounce (0.24 liter), narrow-mouthed glass bottle was charged with 126 g of Norpar™ 12, 14.6 g of EMA, 1.4 g of EA, 7.7 g of the graft stabilizer mixture from Example 1 at 25.98% polymer solids,
25 and 0.18 g of V-601. The bottle was purged for 1 minute with dry nitrogen at a rate of approximately 1.5 liters/minute, then sealed with a screw cap fitted with a Teflon liner. The cap was secured in place using electrical tape. The sealed bottle was then inserted into a metal cage assembly and installed on the agitator assembly of an Atlas Launder-Ometer (Atlas Electric Devices Company, Chicago, IL). The Launder-Ometer was
30 operated at its fixed agitation speed of 42 RPM with a water bath temperature of 70°C. The mixture was allowed to react for approximately 16-18 hours, at which time the

conversion of monomer to polymer was quantitative. The mixture was cooled to room temperature, yielding an opaque white dispersion.

This organosol was designated LMA/HEMA-TMI//EA/EMA (97/3-4.7//13/87 %w/w). The percent solids of the organosol dispersion was determined to be 12.02% 5 using the Halogen Lamp Drying Method described above. Subsequent determination of average particle size was made using the Laser Diffraction Analysis described above; the organosol had a volume average diameter of 1.2 μm .

Example 3

10 This is an example using the graft stabilizer in Example 1 to prepare an organosol with the ReactintTM Urethane Colorant chemically bonded to the organosol. A 5000 ml 3-neck round flask equipped with a condenser, a thermocouple connected to a digital temperature controller, a nitrogen inlet tube connected to a source of dry nitrogen and a magnetic stirrer, was charged with a mixture of 2880 g of NorparTM 12, 341.5 g of EMA, 15 31.8 g of EA, 8.4 g of TMI, 52.5 g of ReactintTM Black X41LV (Milliken Chemical, Spartanburg, SC 29304) and 179.5 g of the graft stabilizer mixture from Example 1 at 25.98 % polymer solids, and 6.30 g of V-601. While stirring the mixture, the reaction flask was purged with dry nitrogen for 30 minutes at flow rate of approximately 2 liters/minute. A hollow glass stopper was then inserted into the open end of the 20 condenser and the nitrogen flow rate was reduced to approximately 0.5 liters/minute. The mixture was heated to 70°C for 16 hours. The conversion was quantitative. The mixture was cooled to room temperature, yielding a self stable black dispersion.

Approximately 350 g of n-heptane were added to the cooled dispersion, and the resulting mixture was stripped of residual monomer using a rotary evaporator equipped 25 with a dry ice/acetone condenser and operating at a temperature of 90°C and a vacuum of approximately 15 mm Hg. The stripped organosol was cooled to room temperature, yielding a stable black organosol.

This organosol was designated LMA/HEMA-TMI//EA/EMA /TMI/ Reactint Black (97/3-4.7//7.3/78.6/12.1/2.0 %w/w). The percent solids of the organosol dispersion 30 after stripping was determined to be 13.91% using the Halogen Lamp Drying Method described above. Subsequent determination of average particle size was made using the

Laser Diffraction Analysis described above; the organosol had a volume average diameter of 2.1 μm .

Example 4

5 This is an example using the graft stabilizer in Example 2 to prepare an organosol with the ReactintTM Urethane Colorant chemically bonded to the organosol and the particle size smaller than 1.0 μm . Using the method and apparatus of Example 1, except a 32 ounce (0.96 liter) glass bottle was used, 536 g of NorparTM 12, 63.4 g of EMA, 5.9 g of EA, 0.78 g of TMI, 9.8 g of ReactintTM Black X41LV (Milliken Chemical,
10 Spartanburg, SC 29304) and 33.3 g of the graft stabilizer mixture from Example 1 at 25.98 % polymer solids, and 1.17 g of V-601 were combined and resulting mixture reacted at 70° C for 16 hours. The mixture was cooled to room temperature.

15 After stripping the dispersion using the method of Example 3 to remove residual monomer, the stripped dispersion was cooled to room temperature, yielding a self stable black organosol.

This organosol was designated LMA/HEMA-TMI//EA/EMA/TMI/ Reactint Black (97/3-4.7//7.4/79.3/12.3/1.0 %w/w). The percent solids of the organosol dispersion after stripping was determined to be 13.69% using the Halogen Lamp Drying Method described above. Subsequent determination of average particle size was made using the
20 Laser Diffraction Analysis described above; the organosol had a volume average diameter of 0.3 μm .

Example 5

This is an example using the graft stabilizer in Example 1 to prepare a black organosol with the ReactintTM Urethane Colorant chemically bonded to the organosol and the particle size larger than 5.0 μm . Using the method and apparatus of Example 2, except a 32 ounce (0.96 liter) glass bottle was used, 534 g of NorparTM 12, 63.4 g of EMA, 5.9 g of EA, 2.34 g of TMI, 9.8 g of ReactintTM Black X41LV (Milliken Chemical, Spartanburg, SC 29304) and 33.3 g of the graft stabilizer mixture from Example 1 at
25 25.98 % polymer solids, and 1.17 g of V-601 were combined and resulting mixture reacted at 70° C for 16 hours. The mixture was cooled to room temperature.

After stripping the dispersion using the method of Example 2 to remove residual monomer, the stripped dispersion was cooled to room temperature, yielding a self stable black organosol.

- This organosol was designated LMA/HEMA-TMI//EA/EMA/TMI/ Reactint
- 5 Black (97/3-4.7//7/78/12/3 %w/w). The percent solids of the organosol dispersion after stripping was determined to be 13.57% using the Halogen Lamp Drying Method described above. Subsequent determination of average particle size was made using the Laser Diffraction Analysis described above; the organosol had a volume average diameter of 8.0 μm .

10

Examples 6-7: Preparation of Liquid Toners.

- For characterization of the prepared liquid toner compositions in these Examples, the following were measured: size-related properties (particle size); charge-related properties (bulk and free phase conductivity, dynamic mobility and zeta potential); and
- 15 charge/developed reflectance optical density (Z/ROD), a parameter that is directly proportional to the toner charge/mass (Q/M).

Example 6

- This is an example of preparing black liquid toner using the organosol prepared in
- 20 example 3. 300 g of organosol in example 3 @ 13.91% (w/w) solids in NorparTM 12 were combined with 2.32 g of 1.00% Zirconium HEX-CEM solution (OMG Chemical Company, Cleveland, Ohio) in a 0.5 liter plastic bottle. The mixture was placed on a shaker for 48 hour before testing.

- A 13% (w/w) solids toner concentrate exhibited the following properties as
- 25 determined using the test methods described above:

- Volume Mean Particle Size: 2.0 micron
Q/M: 447 $\mu\text{C/g}$
Bulk Conductivity: 969 picoMhos/cm
Percent Free Phase Conductivity: 22.9%
- 30 Dynamic Mobility: 5.14E-11 (m^2/Vsec).

This toner was tested using the printing procedure described above. The reflection optical density (ROD) was 0.60 at plating voltages greater than 525 volts. The toner exhibited a good electrostatic transfer efficiency.

5

Example 7

This is an example of preparing black liquid toner using the organosol prepared in example 3. 300 g of organosol in example 3 @ 13.91% (w/w) solids in NorparTM 12 were combined with 4.64 g of 1.00% Zirconium HEX-CEM solution (OMG Chemical Company, Cleveland, Ohio) in a 0.5 liter plastic bottle. The mixture was placed on a shaker for 48 hour before testing.

A 13% (w/w) solids toner concentrate exhibited the following properties as determined using the test methods described above:

Volume Mean Particle Size: 2.0 micron

Q/M: 840 μ C/g

15 Bulk Conductivity: 1443 picoMhos/cm

Percent Free Phase Conductivity: 23.3%

Dynamic Mobility: 6.37E-11 (m²/Vsec).

This toner was tested using the printing procedure described above. The reflection optical density (ROD) was 0.53 at plating voltages greater than 525 volts. The toner exhibited a good electrostatic transfer efficiency.

All percentages and ratios used herein are weight percentages and ratios unless otherwise indicated. All publications, patents and patent documents cited are fully incorporated by reference herein, as though individually incorporated by reference.

Numerous characteristics and advantages of the invention meant to be described by this document have been set forth in the foregoing description. It is to be understood, however, that while particular forms or embodiments of the invention have been illustrated, various modifications, including modifications to shape, and arrangement of parts, and the like, can be made without departing from the spirit and scope of the invention.